

# Modeling and Simulation of an Isolated Site Conversion Chain Driven by a Permanent Magnet Generator

Aicha Wahabi, Abdelhadi El Moudden, Fatima Ezzahra Bounifli, Kaoutar Senhaji Rhazi

**Abstract**—The objective of this work is to study the conversion of wind energy in its entirety in order to optimize the output power and improve the quality of the energy supplied. For this, we are interested in the modeling and simulation of a turbine associated with a speed multiplier, we study the modeling and control of a permanent magnet synchronous generator feeding a three-phase load which corresponds to a chain of Conversion of small-scale wind power into an isolated site. The technique adopted is developed in Matlab / Simulink / SimPowerSystems. The results of the simulation are presented and analyzed at the end of this work.

**Index Terms** — Wind generator - Permanent magnet synchronous generator -Modelization-Matlab Simulink -SimPowerSystems.

## I. INTRODUCTION

Wind turbines based on generators, either asynchronous or with a wound rotor, have the disadvantage of requiring a system of rings and brushes for the doubly fed induction generator (DFIG) and a multiplier for the DFIG and asynchronous squirrel cage machine, resulting in significant maintenance costs, in particular for offshore projects located in saline medium [2],[5],[6]. In order to limit these disadvantages, some manufacturers have developed wind turbines based on synchronous machines with a large number of pole pairs and coupled directly to the turbine, thus avoiding the multiplier. If the generator is equipped with permanent magnets, the system of rings and brushes is eliminated.

The development of magnetic materials allowed the construction of synchronous machines with permanent magnets with costs that become competitive. Machines of this type have a large number of poles and allow the development of considerable mechanical torques [7].

In this article, we study the modeling and control of a permanent magnet synchronous generator driving a small power wind farm for an isolated site. The results of the various simulations of the conversion, carried out in the MATLAB / Simulink environment, made it possible to evaluate the performance of the proposed system.

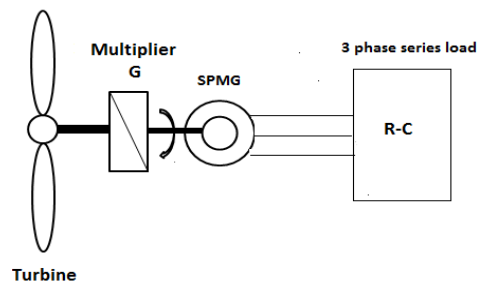
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The coupling of these machines with the power electronics is becoming more and more economically attractive, making it a serious competitor of the doubly fed induction generator.

## II. DESCRIPTION OF THE WIND ENERGY CONVERSION CHAIN DRIVEN BY A SYNCHRONOUS PERMANENT MAGNET GENERATOR "SPMG"

The kinetic energy of the wind is received by the blades of the turbine, transformed into mechanical energy on the turbine shaft, in the form of "slow speed and high torque", it is received by the multiplier which increases the rotational speed and decreases torque. The electric generator, which is here a permanent magnet synchronous generator, transforms the mechanical energy into electrical energy that will feed the load, because we recall that here we are studying a wind energy conversion chain for an isolated site.

The modeling and simulation of the various constituents of the chain will be examined below.



Kinetics Energy → Mechanical Energy → Electric energy

Fig. 1: Simplified scheme of the chain studied

## III. MODELLING OF THE TURBINE

The wind turbine is a device that transforms the kinetic energy of the wind into mechanical energy. The kinetic energy is materialized by the movement of the particles of the mass of air passing through the section of the active surface  $S$  of the wing of the turbine.

By applying the theory of momentum and the Bernoulli theorem we can determine the incident power (theoretical power) of the wind [1], [3].

$$P_{incident} = \frac{1}{2} \rho \cdot S \cdot v^3 \quad (1)$$

$S$ : The surface swept by the blades of the turbine [m<sup>2</sup>];

$\rho$ : The density of air ( $\rho = 1225$  kg / m<sup>3</sup> at atmospheric pressure);

$v$ : Wind speed [m / s].

In a turbine, the power extracted from provided on the rotor of the turbine is lower than the incident power.

$$P_{ext} = \frac{1}{2} \rho \cdot S \cdot C_p(\lambda, \beta) \cdot v^3 \quad (2)$$

$C_p(\lambda, \beta)$ : is the power coefficient which expresses the efficiency of the turbine, it depends on the ratio  $\lambda$ , this ratio represents the ratio of the turbine speed at the end of the blades and the wind speed, and the orientation angle  $\beta$ .

$$\lambda = \frac{R \cdot \Omega_t}{v} \quad (3)$$

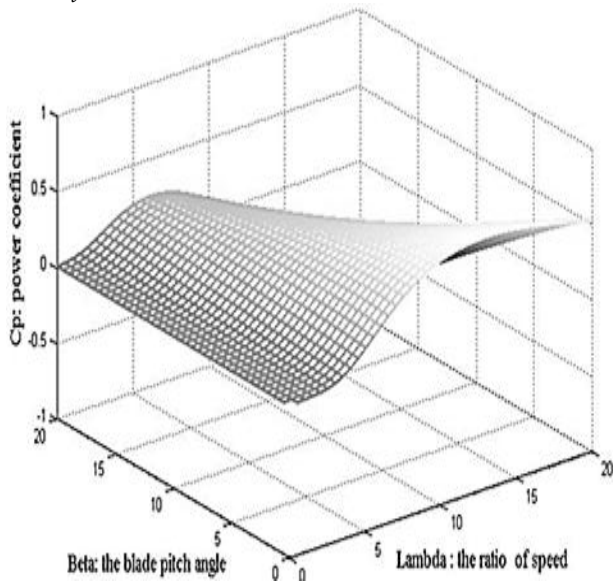


Fig. 2. : Power coefficient  $C_p(\lambda, \beta)$

The maximum power coefficient  $C_p$  was determined by Albert Betz (1920) as follows:

$$C_p^{max}(\lambda, \beta) = \frac{16}{27} \approx 0,593 \quad (4)$$

This coefficient depends on the constitution of the turbine, for a wind medium power we have:

$$C_p(\lambda, \beta) = c_1 \cdot \left( c_2 \cdot \frac{1}{A} - c_3 \cdot \beta - c_4 \right) \cdot e^{-c_5 \frac{1}{A}} + c_6 \cdot \lambda \quad (5)$$

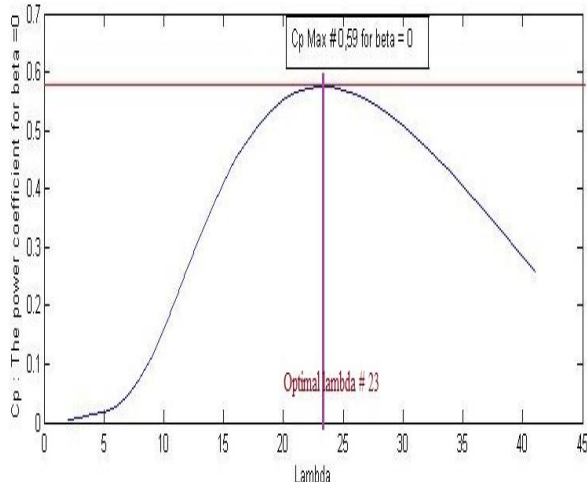


Fig. 3:  $C_p$  Power coefficient for  $\beta = 0$

Also, we can say that this turbine will present its maximum efficiency for a speed ratio  $\lambda$  [1] [2], of the order of 23 since in general,  $C_p$  is maximal for  $\beta = 0^\circ$

If the velocity ratio  $\lambda$  is maintained at its optimum value  $\lambda_{opt}$ , the coefficient of power is at its maximum value  $C_{pMAX} = C_p(\lambda_{opt})$ , the maximum of power of the wind

turbine [4] is:

$$P_{opt} = \frac{1}{2} \rho \cdot S \cdot C_{pMAX} \cdot v^3; \text{ with } v = \frac{R}{\lambda_{opt}} \cdot \Omega_t \quad (6) \text{ So } P_{opt} = \frac{1}{2} \rho \cdot S \cdot C_{pMAX} \cdot \left( \frac{R}{\lambda_{opt}} \cdot \Omega_t \right)^3 \quad (7)$$

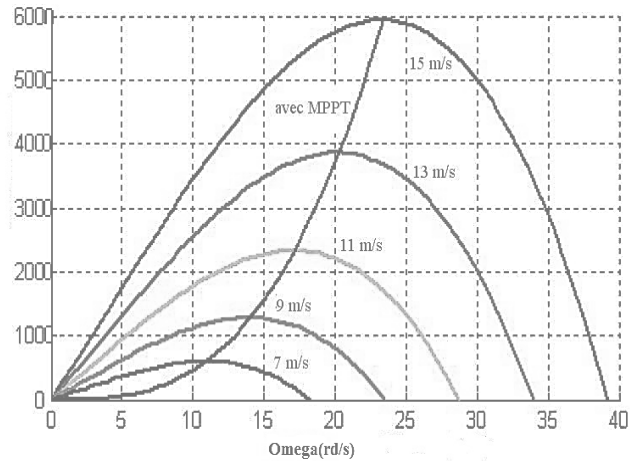


Fig. 4: Wind Power (W) for several wind speed and  $\beta = 0$

We note that the wind power is very affected by the variation of  $v$ : the wind speed, because the coefficient  $C_p$  depends on  $\lambda$  therefore of  $v$ , and from the relation

$P_{ext} = \frac{1}{2} \rho \cdot S \cdot C_p(\lambda, \beta) \cdot v^3$ , we see that the power is proportional to the cube of the wind speed. Moreover, it is noted that the maximum power extracted varies as a function of the wind speed, hence the advantage of using for a large plant a generator which adapts to the wind speed the “DFIG” (Doubly Fed Induction Generator) which is the most Able to extract at each moment the maximum power [ ].

$C_t$  is the torque on the slow axis at the turbine:

$$C_t = \frac{P_{ext}}{\Omega_t} = \frac{1}{2} \rho \cdot S \cdot C_p(\lambda, \beta) \cdot v^3 \cdot \frac{1}{\Omega_t} \quad (8)$$

The total inertia  $j$  consists of the inertia of the turbine  $j_t$  reduced the fast axis and the inertia of the generator  $j_g$  :

$$j = \frac{j_t}{G^2} + j_g \quad (9)$$

The fundamental equation of dynamics can be written:

$$j \frac{d\Omega_{Mec}}{dt} = C_M = C_t - C_{em} - f \Omega_{Mec} \quad (10)$$

#### IV. MODELLING OF SYNCHRONOUS PERMANENT MAGNET GENERATOR “SPMG”

Thanks to the advantages it offers compared with other types of electrical machines (not requiring magnetization, performance, robustness, etc.), the permanent magnet synchronous machine is advantageous for a generator application coupled to an isolated wind turbine.

To model and control a permanent magnet synchronous generator, the model of the most appropriate machine and for the implementation of the control laws is inspired by the work [1],[3],[4].

For the 3-phase stator, this writing is summarized by the following condensed matrix:

$$[V_{sabc}] = [R_s] * [i_{sabs}] + \frac{d}{dt} [\Phi_{sabc}] \quad (11)$$

With  $[V_{sabc}]$  : three-phase stator voltage of the synchronous machine.  $[R_s]$  : Resistance of stator phase.  $[i_{sabs}]$  : Three-phase stator current of the synchronous machine.  $[\Phi_{sabc}]$  : Feed-phase stator of the synchronous

machine.

We will use the Park model of this machine. The equations of the machine in the referential two-phase of Park are the following [ ]

$$V_{sd} = R_s * i_{sd} + L_s * \frac{di_{sd}}{dt} - L_s * i_{sq} * \omega \quad (12)$$

$$V_{sq} = R_s * i_{sq} + L_s * \frac{di_{sq}}{dt} + (L_s * i_{sd} + K_A) * \omega \quad (13)$$

$$C_{em} = p * K_A * i_{sq} \text{ And } \omega = p * \Omega \quad (14)$$

$V_{sd}, V_{sq}$  and  $i_{sd}, i_{sq}$ : are the stator voltage and stator current in the two-phase reference.

$C_{em}, p$ : Are the electromechanical couple and the number of pairs of pole,  $L_s$ : cyclical inductance of a stator phase.

V. SIMULATION OF THE CHAIN STUDIED

We have placed the different constituents of the chain and we connected them and simulated them. After some adjustments, the system works correctly. The results of the simulation will be presented and interpreted in the following paragraph.

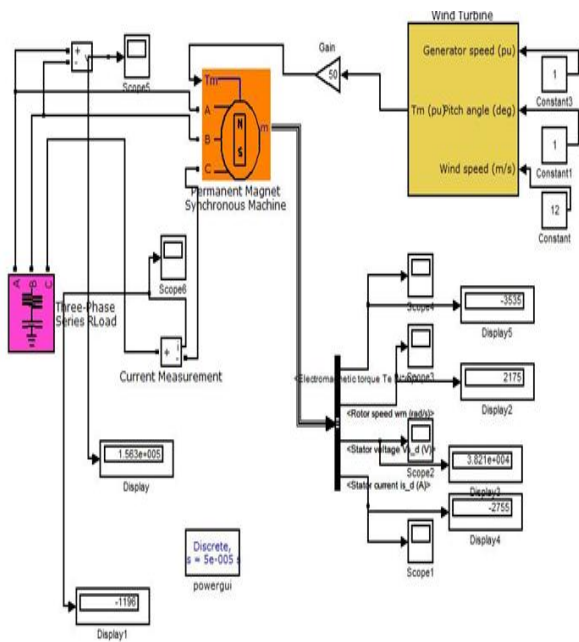


Fig. 6: Block diagram of the wind chain driven by permanent magnet generator.

A. Simulation results

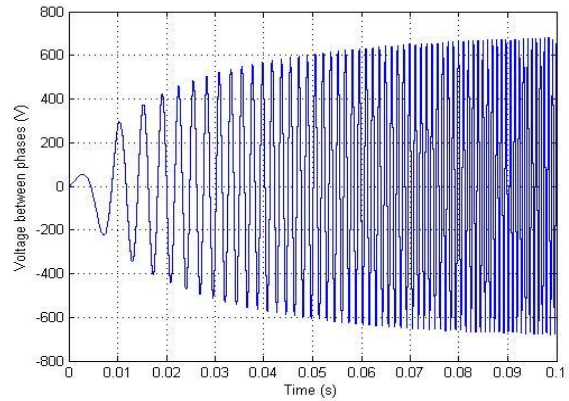


Fig.7 : Variation of stator voltage between phase as a function of time

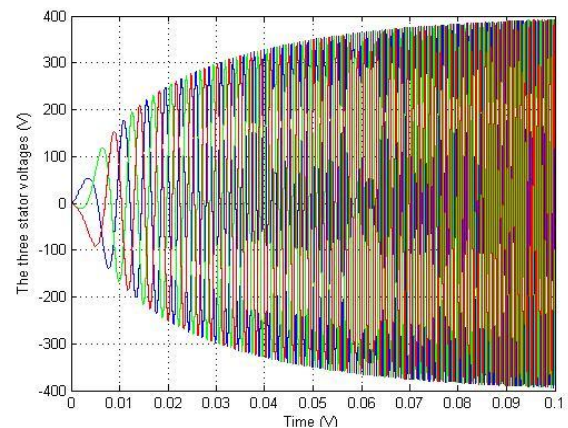


fig. 8 : Variation of the three stator voltages as a function of time.

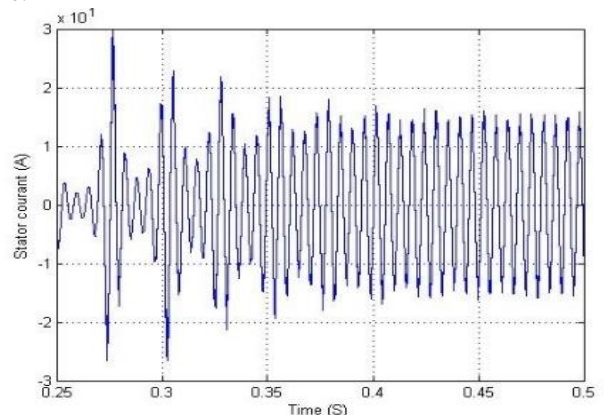


Fig. 9a. Stator current in transient mode

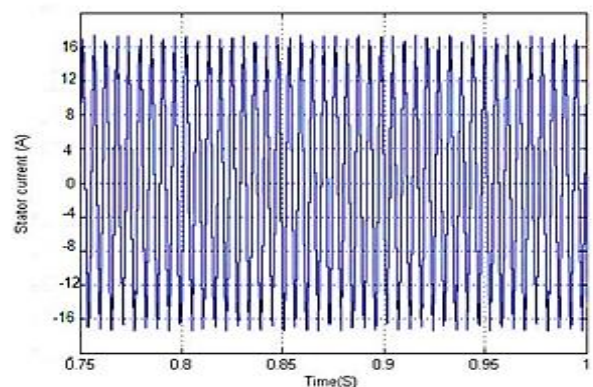


Fig. 9b. Stator current during steady state



VI. CONCLUSION

In this article, we recalled the mathematical models of the components of the wind energy conversion system (turbine models, permanent magnet synchronous machine).

The results of the simulation carried out for the different models allowed to validate the proposed mathematical models of the wind system.

We will improve this work in order to have a constant value of the active power produced and the speed of rotation by inserting filters to minimize the fluctuations of these two curves.

We also plan to study a chain driven by the same generator but avoiding the multiplier since there are machines with a very high number of poles.

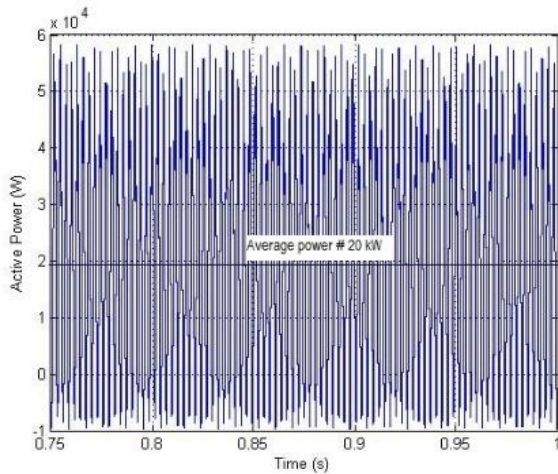


Fig. 10. Total active power produced by the chain

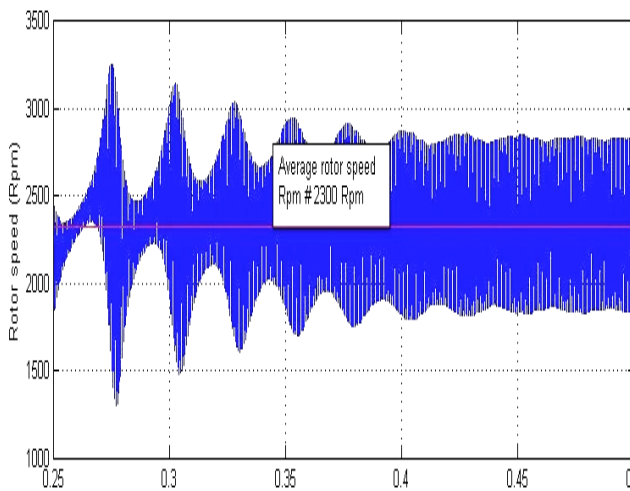


Fig. 11. Rotor speed in Rpm

B. Comments and Discussions

The results presented above show that the chain was correctly modeled and simulated, indeed the flow of energy received by the turbine was actually sent to the electric generator to supply the load with electrical energy.

Fig 7 and 8 show the stator voltages supplied by the generator. These are sinusoidal voltages of period  $T = 0.02s$  which correspond to a frequency of 50 Hz of maximum values  $V_{max} \approx 400V$  for the phase-to-neutral voltage (680V for the compound voltage) this is an acceptable voltage because the chain studied corresponds to an installation in an isolated site of average power and it is the voltage that is generally adopted.

Fig. 9a and 9b show the line current supplied by the generator in transient and permanent condition. It is a sinusoidal current of period  $T = 0.02s$  also which correspond to a frequency of 50 Hz. The maximum value is  $I_{max} \approx 16A$ .

Fig.10 shows the variation of the total active power supplied by the wind system. We note that the power delivered is considerable and that it is subjected to fluctuations. It can also be said that the average power delivered is of an average value of 20 kw.

The last figure gives us an idea of the speed of rotation of the generator which is almost equal to 2300ppm (we added a multiplier to have the unit ppm) one notices that the rotation speed also undergoes fluctuations.

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